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## Design and Development of Different Applications of PATB (Porous Aerostatic Thrust Bearing): A Review

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### ABSTRACT

In several applications demanding precise and ultra-precision movements, porous aerostatic thrust bearings had been employed as a crucial precision engineering component and enabling technology. By acting as a lubricant between the moving part and the stationary part in aerostatic bearings, pressurized air almost completely eliminates friction. Since air acts as the lubricant, oil-based lubricants leave no debris behind. The air prolongs the life of the substances by preventing them from slipping and wearing. The aerostatic type uses graphite as a porous film to disrupt the air uniformly over the surface, or a tiny hole is drilled through the centre of the bearing to let the air circulate and produce a thin layer between the components. With an increased reliance on computational and mathematical methodologies for design and bearing performance optimization, this review paper aims to present the state-of-the-art in aerostatic bearings advancement and research. It also conducts a critical analysis of their future research directions and development trends in the next ten years and beyond. Air bearings are utilized in the production of tools like lathes, CMM, and grinders because they are highly precise in their operation and decrease mistakes and production time. Air bearings are available in a variety of forms and sizes. The assessment of future trends and obstacles in aerostatic bearings investigation, as well as their prospective applications in the precision engineering sectors, concludes the study.

**Keywords:** Aerostatic bearing; Porous layer; Thrust bearing; Precision motions.

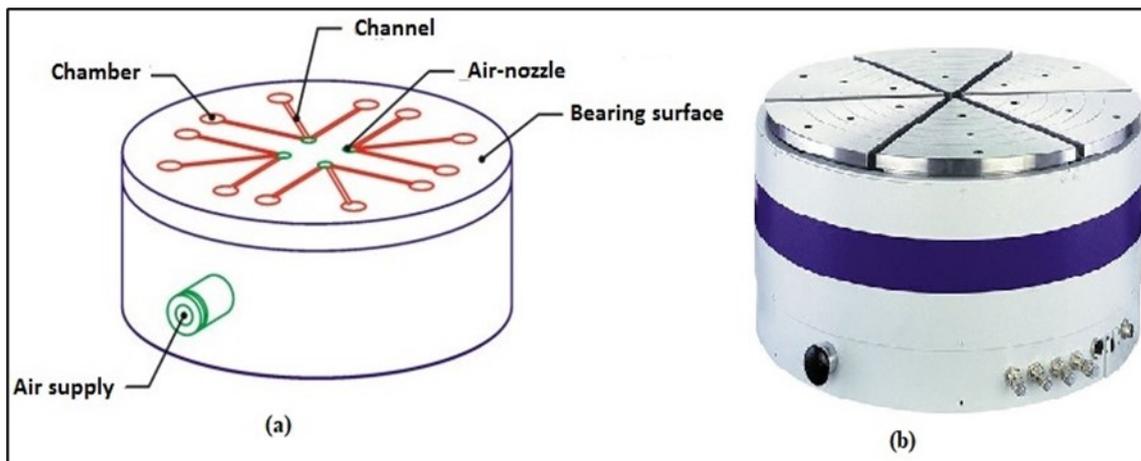
### Introduction

Due to the simplicity of using porous material to create an aerostatic bearing, aerostatic porous bearings have been effectively used in precision machine tools and precision measurement equipment. Recently, improved ceramics and graphite, which can attain a modest permeability in the range of 10-15 m<sup>2</sup>, have frequently replaced metal in porous materials. This is due to the fact that employing porous material with a reduced permeability makes it simple to get a greater bearing stiffness [1-2]. The aerostatic bearings, which have been widely used in a variety of applications, including the manufacturing of semiconductors, medical devices, ultra-precision measuring, turbomachinery, machining equipment, etc., use a pressurised thin air film of micron-level thickness to support the moving objects. Some properties of aerostatic bearings are low friction, precise rotation, and ultra-precision. In order to fulfil the needs for enhanced performance in associated sectors such as semiconductors, defence, microelectronic, textile, aerospace, and measuring instruments, extensive research has been undertaken on the performance of aerostatic

thrust bearing [3-5].

Aerostatic bearings serve two primary purposes, namely, the minimization of friction and motion faults. The stiffness, static properties, and load-carrying capacity of aerostatic thrust bearings have all been explored in earlier works. The features of aerostatic porous bearing with something like a surface-limited layer have been published by a number of studies. Aerostatic circular porous thrust bearings were treated with a surface limited layer by Yoshimoto [6]. They looked into the static and dynamic properties of this particular type of graphite bearing both theoretically and empirically. They also presumptively believed that Darcy's law applies to airflow in a surface limited layer. However, because a limited layer was often very thin, the radial flow and porosity in it were considered to be zero in their calculations.

Yabe et al. [7] employed porous metal with a limited layer created using a surface grinder to treat an aerostatic circular porous thrust bearing. For the situation of a reasonably large bearing clearance of some more than 20 mm, where the dynamic characteristics are not significantly



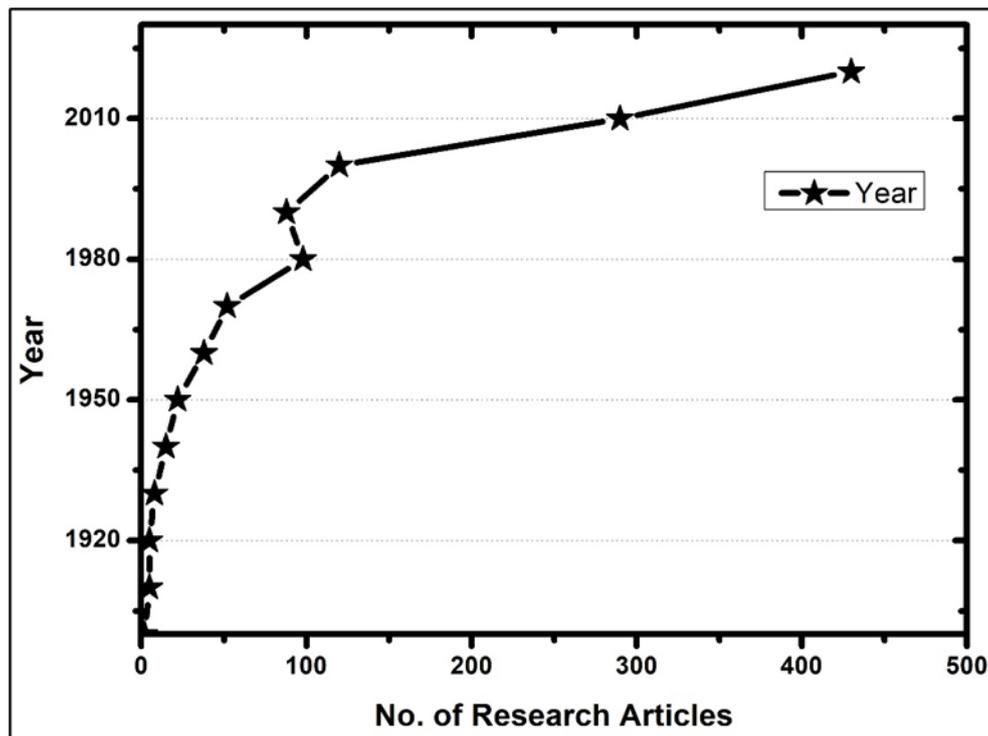
**Figure 1:** Aerostatic Journal Bearing (a) Schematic View (b) Original View [79]

impacted by the squeezing effect, they reported the theoretically predicted and empirically determined dynamic characteristics of this type of bearing. They discovered that theoretical conclusions drawn from their comparable clearance model were in good accord with the findings of the experiments. An aerostatic annular porous thrust bearing made of surface-restricted graphite was researched by Cui and Ono [8]. The permeability of this porous substance is approximately one-tenth of that of the porous metal that Yabe et al. [7] studied. As a result, they looked at the bearing properties in a limited (10 mm or less) bearing clearance range. Lacquering was used to create the surface-restricted layer of porous graphite material. Using a perturbation approach, Kawashima and Togo et al. [9] theoretically examined the static properties of aerostatic porous ceramic journal bearings. They also applied a confined layer to an aerostatic porous journal bearing; however, they simply displayed the pressure gradient in the porous material.

The techniques of annular groove air supply and entire air supply, which were employed to prevent the deflection of the bearing surface of aerostatic circular porous thrust bearings, were researched by Yoshimoto et al. [10]. Otsu et al. [11] evaluated the dynamic stiffness and damping coefficient of aerostatic porous journal bearings and also demonstrated that raising the permeability and lowering the small surface restriction ratio can result in higher dynamic stiffness and a higher damping coefficient. The micro-vibration of aerostatic thrust bearings with surface limitation provided by T-shaped grooves was explored by Yoshimura et al. [12]. They found that the Reynolds number at the bearing outlet significantly affected the nano-fluctuation of aerostatic bearings. According to research, restrictors made of porous material with permeabilities in the order of  $1e-15 \text{ mm}^2$  can reach the ideal bearing clearance of less than 10  $\mu\text{m}$ , which corresponds to the maximum static stiffness. This can increase the stiffness and stability of aerostatic porous bearings. Aerostatic bearings' stiffness and stability are both governed by the internal pressure distribution in the bearing clearance, and the manufacturing flaws have an impact on the thickness of the bearing clearance. Therefore,

the effects of manufacturing mistakes cannot be disregarded, particularly in gaps with thinner film. Since 1828, when Willis [13] conducted an experimental investigation into the airflow state between two parallel plane surfaces, air lubrication technology has been a growing field. Kingsbury [14] tested the supporting properties of an air journal bearing near the end of the 19th century, confirming the viability of gas bearing. Then, in the early 1900s, several patents relating to gas bearings were granted [15]. Instances include the air thrust bearing developed by Westinghouse [16] in 1904 and the aerostatic journal bearing developed by Abbott [17] in 1916. However, very few studies pertaining to the fundamentals of gas lubrication were documented in the next decades [18]. Figure 2 displays the Scopus [19] document search results for the keywords "air bearing or gas bearing." Due to demands from the nuclear power and defence sectors, gas lubrication technology initially took off in developed nations like the United States during World War II [20]. Aerostatic bearings have been invented, produced, and extensively used in a variety of sectors since their specific inception, including high-speed dentistry drills [17], space simulators [18], precise machine tools, and measurement equipment [19]. It clarifies the cause of the first discernible upward trend from 1960. Numerous monographs on gas lubrication technology were produced during the 1970s and 1990s, which denotes a mature time for its design theory [13–21]. The top ten nations in terms of air-bearing research are listed in Fig. 2. It is clear that the United States, China, Japan, and other countries hold the top spot. The top 10 nations in gas bearing research are also nations with strong needs for ultra-precision machinery, confirming the importance of gas bearings as essential parts of ultra-precision machinery.

Aerostatic bearings have been known to employ porous materials as restrictors in the past. Its improved damping properties, larger load capacity, rigidity, and ease of design and fabrication over traditional restrictors are only a few of its numerous benefits [22]. It is simple to obtain even complex bearing geometries like spherical bearings and aerostatic lead screws [23]. Numerous bearing geometries have been covered in the theories of porous aerostatic



**Figure 2:** Annual documents quantity of articles related to air bearings by searching with keywords of 'air bearing' in Scopus.

bearings. Two bibliographic evaluations are among the numerous publications; the first was written by Sneek in 1968 [24]. Majumdar subsequently modified this in 1976 [25]. The foundations of porous aerostatic bearings had previously been established in published literature at that point, comprising one-dimensional analytical models and two-dimensional calculations with adjustment for compressible, slip, and inertia flows. Theoretical and experimental research has also been done on dynamic and stability properties. The majority of these papers made the assumption that Darcy's rule applied to flow through porous media.

After 1976, a sizable amount of work was also recorded, particularly more recently as a result of rekindled interest in Japan and Germany. Two primary streams can be formed from them. Several theoretical investigations, including three-dimensional numerical assessments on rectangular thrust bearings that contain additional factors such as permeability anisotropy, tilt, slip flow, offset load etc., have been the focus of a group of researchers in India.

To produce load-bearing capacity, air bearings need an external high-pressure air supply. Air pressure between 400 and 600 kPa, which is what is generally employed in the sector, is used in the majority of air-bearing applications. The input pressure is rather low, which limits the load-carrying capability. Using a specialised compressor, air bearings may be used in sensitive applications with pressures of up to 1000 kPa. This increases load-bearing capacity and rigidity [28]. In comparison to other bearing ideas, the air bearing offers significant benefits such as extremely low friction, minimal

wear, and wide range of working speed [29–30]. The air bearing is a part that is utilised in the construction of ultra-precise machinery. It works incredibly well in absorbing vibrations from the environment [31]. There is very little space between the components and the bearing, which is the fundamental drawback of air bearings. As a result, it needs extremely tight tolerances. It requires compressed air to operate continuously. Air bearings are also not very rigid. However, preloading the bearing can greatly boost rigidity. Preloading air bearings can be done in four ways: weight addition, magnetic attraction, opposing assembly, and vacuum preloading. The vacuum preloading approach is popular since it is small and does not add additional weight [32–33]. To accomplish uniform air distribution to the contact surface and uniform pressure distribution in the air bearing, a porous material is employed [34–35].

The review discussed on this page includes theoretical and experimental research, as well as the major conclusions drawn from them, which are mostly based on the many invented bores. Additionally, several materials used in the fabrication of PATB's components as well as their production processes, have been shown and explored. Additionally, each part offers evaluations in the way of the authors' current examinations, remarks, and potential future paths. In a few instances, it has been discovered that refrigerants, oils or lubricants have already been utilised in compliant bore journal bearings in place of air. As a result, this article has also covered these bearings' performance characteristics. For the convenience of the researchers, a summary of the review and the potential areas for further investigation are provided at the conclusion of this article.

**Table 1:** Materials used in an aerostatic bearing by different researchers.

Materials Used	Reference No.
Diamond-like-carbon (DLC)	[68]
Chromium	[56, 61,76]
Inconel 618	[54]
Cr-Mb steel	[62-64]
Inconel 718	[56-58]
Molybdenum	[36]
AISI 304	[49]
MoS <sub>2</sub>	[43,81]
Inconel Alloy 625	[55]
AISI 4340	[81]
Beryllium Bronze (QBe2.0)	[66],
42CrMo4	[39]
Inconel 718	[28-30,41,45,49, 56,61,79,80]
PS400	[81]
AISI 4140	[42,62,73,82]
Stainless steel	[68]
PS304	[24,43,71,72,83,84]
UNS S17400	[67]
Beryllium Bronze (QBe1.8)	[65]
AISI 301	[59,60]
Amorphous M	[27,30]
AISI 316	[61]
Inconel X-750	[43-74]

### Materials used in the fabrication of PATBs

Since the air film's pressure is produced by an external air supply system, aerostatic bearings are also known as externally pressurized air bearings. Through a specialized restrictor, pressurized air is introduced into the space between two bearing surfaces, and from the exit edges of the bearing clearance, it is released into the ambient environment. In the space between fixed and moving pieces, the thin layer serves as a lubricant. Since the moving and stationary surfaces of an air bearing are not in touch while it is operating, it not only avoids numerous issues common to traditional bearings, like wear and friction but also has unique advantages for precise placement.

The characterization of coated layers on the journal substrates and upper foil is offered after a study of the materials used in making the various PATB components. Near the end of this part, the fabrication processes for the bearing components were covered. According to a literature review, the journal/rotor as well as the sleeves, are often made from the same materials. Moreover, to reduce tribological issues and boost heat dissipation during starts and stops, hard-coated layers have been placed on the top-compliant foil or journal and bearing surface. To give resistance to fatigue and extra dampening to the system, compliant journal-bearing surfaces should have good elastic behaviour and increased heat conductivity. To create the traditional stiff PATBs and the rotors, the researchers employed high carbon chromium (AISI 52100) alloy steel [36]. The rotors and PATBs have also been constructed using stainless steel-(AISI TY416) and toughened steel [37-39]. Additionally, sleeves for the PATBs have also been made using stainless steel-(SAE/AISI 316 L) [40]. Graphite has been put on the PATBs to enhance their tribological behaviour. Additionally, it was

discovered that bronze was used in the manufacturing of both the standard and herringbone grooved stiff PATBs' sleeves [38, 41, 42].

To reduce wear and improve heat dissipation rate during rotor start and stop, several coating materials were applied to the PATB bore/rotor surfaces. The compliant-bore surfaces were made using a variety of materials with strong elastic and damping capabilities. The dynamic and tribological performances of PATBs have been compared, but little study has been done to compare them when the materials for the compliant surface, sleeve, coating, and rotor are changed. The functioning of rotors sustained by PATBs during frequent stop/start and extended running circumstances with various factors was also the subject of few research, which has been reported.

### Operating Conditions for PATB:

The gas film clearance is often less than 10  $\mu$ m, which is quite small. Accurate measurements of the pressure distribution in the bearing clearance might be challenging to achieve. There are two primary ways to assess pressure distribution. To detect the pressure distribution in the gas film, the pressure sensor is first connected to the orifice. On one of the pad's surfaces, the orifice is drilled [56]. In the literature, this tiny aperture is referred to as the flow intake ( $d_p = 0.2$  mm) [58]. This method's pressure distribution and the outcomes of the numerical simulation are in good accord. Although, there are still certain drawbacks to the approach used to connect the pressure sensor to the orifice plate. Secondly, there are noticeable and not insignificant changes to the airflow in the small gap, as well as significant measurement errors. Moreover, the number and location of experimental data that may be collected using this approach are also constrained [112].

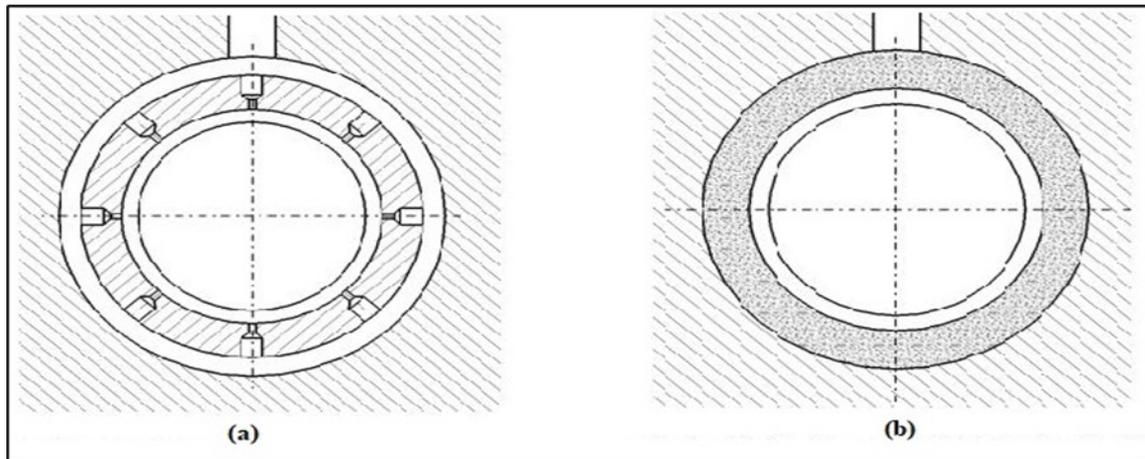


Figure 3: Aerostatic Thrust Bearing (a) with a simple orifice (b) with a porous layer [111]

### Theoretical Research on PATB:

The previous research on theoretical modelling methods and related performance evaluations of aerostatic bearings under continuously loaded situations is reviewed in this part, along with a few notable works that represent state-of-the-art investigation in this field. This section discusses the evolution of research on various PATBs (as shown in Fig. 3).

Malanoski [37] solved the numerical simulations to determine the radial stiffness and the system critical mass using FDM and Runge-Kutta (4th Order) techniques. With modifications in rotating speed, the stability zones were demonstrated. Using FEM and the perturbation approach for discretization, Bonneau and Absi [83] and Faria [84] observed the alterations of stiffness coefficients of bearing with variations in eccentricity ratio, compressibility number, groove depth, and groove angle. By using the time marching approach, Kim et al. [85] showed a significant increase in stability by employing axial grooves at the beginning of each stage in a multi-stepped PATB. Critical mass, critical frequency, and stability zones for the helical grooved PATB (conical) or rotor system have been shown by Pan and Kim [86] using variations in compressibility number. In the instance of the herringbone grooved PATB, Chu et al. [87] utilised the perturbation approach and FEM for discretization, and the results demonstrate enhanced dynamic coefficients when compared to plain bore PATB under lightly loaded conditions. By taking into account lobbed bore geometry and the time marching approach, Rashidi et al. [88] have observed periodic responses and multi-periodic responses of the journal centre. By maximising geometric/operating characteristics, Schiffmann and Favrat [89] decrease windage losses and increase stability margin. In order to increase the rotor critical speed, the ideal groove dimensions have been proposed by Miyanaga and Tomioka [90]. According to Guenat and Schiffmann [161], herringbone grooved journal bearings, as compared with plain journal bearings, are more susceptible to moist air. The load-carrying capacity, which has improved with an expansion in the contact area between leaf foils, was

determined using FDM by Du et al. [91] and Li et al. [92]. When the couple-stress parameter was increased, Laouadi et al. [93] observed that the peak pressure, altitude angle, frictional losses, and side leakage were all reduced. In order to solve the modified Reynolds equation, Bonello [94] used FEM and FDM. He then noticed that the clamped free or leading trailing edge of the top foil combination produced a uniform film thickness in the diverging zone, which produced atmospheric pressure. The implications of friction and partings along bump foil-top foil and sleeve-bump foil have been studied by Gu et al. [95]. The model's output has been contrasted with the experimental data and previously published models, and any differences have been explained. Baum et al. [96] found that the suggested model is very computationally productive in respect of accuracy and time by using FEM and Galerkin's approach to determine pressure distribution, load-displacement curves, solution accuracy, and simulation time. The 3D deformation simulations of top or bump foil, bearing sleeve, contact between the bump and top foil, FEM approach, and misalignment for discretization have been studied by Yongpeng et al. [97] and Zhao and Xiao [98]. They discovered that at the diverging area of the film, the top foil is momentarily disconnected from the assisting bump foil. By using the perturbation method and the FEA method, Howard et al. [49] assessed the bearing dynamic coefficient and noted that as the groove depth increased and the damping coefficient across the trend of the external load increased, whereas the coefficient decreased as it is perpendicular to the external load.

### Experimental Research on PATB:

External damping is a useful technique for reducing the large amplitude vibrations, according to a literature review on the experimental investigation of the rotor's dynamic characteristics, which is supported by conventional rigid bore PATBs [7-31]. The gas/air film's direct damping coefficients are improved by external damping. The air/gas film's cross-coupled stiffness allowed dissipation forces to work in opposition to the unstable tangential forces generated. The generated tangential force aids in reducing

rotor vibrations. In this part, a summary of the experimental study work carried out by several tribologists is presented.

To determine power loss, Radil and Dellacorte [99] assessed frictional torque. Then they showed a 3D map in case of power loss with respect to various rotating speeds and external loads. According to Li et al. [100]'s observations, the vertical eccentricity increases as the bearing load increases while decreasing as the rotating speed increases. Employing the piezoelectric actuator frequency and voltage, Ha et al. [101] examined the floating height and discovered that when the piezoelectric actuator voltage was raised, the squeezing film pressure at zero rotating speed increased the floating height of the journal. The viability of the function of the compression spring-supported PATB has been shown by Song and Kim [102]. After the rotor is in the air, Andres et al. [103] monitored the bearing torque with the temperature increase. As the rotating speed and applied load have grown, so have the frictional torque and bearing temperature. In the lengthy steady-state procedure, Feng et al. [104] noticed that the bearing temperature (measured using a thermocouple) had achieved a saturation level. Mahner et al. [105] discovered that an increase in the external load led to an increase in the component assembly temperatures. Eddy current displacement sensors were used by Li et al. [106] to test load-carrying capacity and bearing clearance, and the results were compared to data from theoretical model simulations. According to Andres et al. [103], the breakaway torque has grown with the rotor's speeds during start-up and lift-off and also with the rise in the external load. In order to benchmark the results from theoretical analysis, Lee et al. [79] and [103] conducted load-deflection tests, rotor constant-speed tests, and coast-down tests. They also assessed transient temperature values. They also noticed that the stiffness values increased as well when the density of the metal mesh rose. When compared to older, bump-type PATBs, the new bore PATB (with metal mesh compliant) exhibits better damping properties. Among other tests, Andres and Chirathadam [103] carried out a load-deflection test, a coast-up and coast-down test, and a dynamic shaker test. The foil metal mesh bearing has exhibited less frictional power and airborne torque, more energy dissipation, and an earlier lift-off speed than the traditional bump-type PATB. PATB with several leaves that is compliant was studied by Tian et al. [31] and found to have essentially consistent BDCs over the perturbation frequency range. Electronic actuators have been employed by Feng et al. [68] to adjust the bore geometry. The driving actuator voltage has grown along with the airborne drag torque. Guan et al. [108] noted that the piezoelectric actuators' supply voltage might be adjusted to reduce sub-synchronous vibrations. According to Hu et al. [109], the bump-type shim foil-supported new bore-compliant PATB has produced a smaller rotor orbit (with less vibration in both directions) than a traditional bump-type PATB. In comparison to traditional bump-type PATBs, the rotor supported on the

innovative bore bearing exhibits significantly reduced sub-synchronous vibrations, according to Liu et al. [91]. By adding dampening, the metal mesh blocks' enhanced mesh density has resulted in less sub-synchronous vibration amplitudes. However, thorough three-dimensional numerical formulations for the operation of bump-type refrigerant-lubricated journal bearings have been introduced, and the tribo-dynamics of these kinds of bearings have been studied by the authors [110]. These formulations incorporate thermal, eddy viscosity, turbulence effects, and vapour/liquid transition.

## Conclusions and Future Scope:

It is well acknowledged that research is being conducted worldwide to investigate and enhance the load-carrying capacity, rotor dynamics, and tribological performances accompanied by compliant and rigid bore PATBs. Additionally, it has been shown that operations at low eccentricity ratios make the rotors sustained by rigid bore PATBs susceptible to dynamic instabilities. Based on the review of the literature on porous thrust aerostatic journal bearings provided in this article, the key points observed from the literature review are listed below:

- When determining the tribo-dynamic performance of PATBs, factors such as bearing bore geometry, operating circumstances, and clearance are crucial.
- Many unique compliant bore geometries that provide compliance throughout the operations have been proposed in previous research.
- Furthermore, the clearance change caused by the thermal expansion of bearing parts has been taken into consideration in the design of PATBs.
- However, limited numbers of literatures can be found on the tribological and experimental investigations of novel aerostatic journal bearings.
- When employing PATBs, self-excited sub-synchronous rotor vibrations and nonlinear dynamic performance are perceived.
- The tribological experimental investigations of novel PATBs are understudied.
- The ability to carry higher load for long time is improved by the increase in air viscosity that occurs when the ambient temperature rises.
- The capacity to carry the loads is negatively impacted by rarefaction, which is further encouraged by a rise in the ambient temperature.

There is a need for more investigation into how to use surface texture technologies to minimise friction and wear. It is necessary to conduct experimental research on the newly described compliant bore geometries to comprehend the tribological behaviours under various operating conditions. Compliant bore bearings/ conical aerodynamic

rigid, which can handle both radial and axial thrust simultaneously, have not been the subject of any study. To determine its feasibility, thorough research is needed.

## References:

- [1] Yabe, H., Kitamura, T., and Mori, H., 1981, "A Study on Fundamental Characteristics of Externally Pressurized Porous Thrust Gas Bearings," *ASME J. Sol. Energy Eng.*, **26**, No. 1, pp. 49–55
- [2] Kawashima, I., Togo, S., Sato, S., and Tamada, N., 1990, "Study on Characteristics of Porous Ceramic Gas Bearings," *J. Soc. Precis. Eng.*, **56**, No. 10, pp. 1853–1858.
- [3] Cui, C., and Ono, K., 1997, "Theoretical and Experimental Investigation of an Externally Pressurized Porous Annular Thrust Gas Bearing and Its Optimum Design," *ASME J. Tribol.*, **119**, No. 3, pp. 486–492.
- [4] Iwato, T., and Yoshimoto, S., 1996, "Static and Dynamic Characteristics of circular Aerostatic Porous Thrust Bearing," *Trans. Jpn. Soc. Mech. Eng., Ser. C*, **62**, No. 539, pp. 276–283.
- [5] Gargiulo, E. P., and Gilmour, P. W., 1968, "A Numerical Solution for the Design of Externally Pressurized Porous Gas Bearing: Thrust Bearings," *ASME J. Lubr. Technol.*, **90**, No. 4, pp. 810–817.
- [6] Kohno K, Yoshimoto S. Static and dynamic characteristics of aerostatic circular porous thrust bearings (effect of the shape of the air supply area). *Journal of Tribology* 2001; 123: 501–8.
- [7] Otsu Y, Miyatake M, Yoshimoto S. Dynamic characteristics of aerostatic porous journal bearings with a surface-restricted layer. *Journal of Tribology* 2011; 133:011701.
- [8] Yoshimura T, Hanafusa T, Kitagawa T, Hirayama T, Matsuoka T, Yabe H. Clarifications of the mechanism of nano-fluctuation of aerostatic thrust bearing with surface restriction. *Tribology International* 2012; 48: 29–34.
- [9] Durazo-Cardenas IS, Corbett J, Stephenson DJ. Permeability and dynamic elastic moduli of controlled porosity ultra-precision aerostatic structures. *Ceramics International* 2014; 40: 3041–51.
- [10] Willis R. On the pressure produced on a flat surface when opposed to a stream of air issuing from an orifice in a plane surface. *Trans Camb Phil Soc* 1828;3 (1):121–40.
- [11] Kingsbury A. Experiments with an air-lubricated bearing. *J Am soc Nav Eng* 1897;9(2):267–92.
- [12] Majumdar BC. Externally pressurized gas bearings: a review. *Wear* 1980;62(2):299–314.
- [13] Westinghouse G. Vertical fluid-pressure turbine. U.S. Patent 754 1904;400. 3-8.
- [14] Abbott Jr. WG. Device for utilizing fluid under pressure for lubricating relatively movable elements. U.S. Patent 1 1916;185(571):5–30.
- [15] Wang Y. Gas lubrication theory and gas bearing design. Beijing: China Machine Press; 1999. p. 1–3.
- [16] 'AIR BEARINGS HISTORY' by Bently Bearings, <https://bentlybearings.com/air-bearings-history/>
- [17] Slocum AH. Precision machine design. Society of Manufacturing Engineers; 1992. p. 580–1.
- [18] Powell JW. Design of aerostatic bearings. Brighton: Machinery Publishing; 1970. p. 15–6.
- [19] Powell JW, Maye HH, Dwight PR. Fundamental theory and experiments on hydrostatic air-bearings. *Proc Lubrication and Wear Conv* 1963:23–5.
- [20] Wilcock DF. Design and performance of gas-pressurized, spherical, space-simulator bearings. *J Basic Eng* 1965;87(3):604–12.
- [21] Wunsch HL. The design of air bearing and their application to measuring instruments and machine tools. *Int J Mach Tool Des Res* 1961;1:198–212.
- [22] Gross WA, Matsch LA, Castelli V, Eshel A, Vohr JH, Wildmann M. Fluid film lubrication. United States: N. p.: Web; 1980.
- [23] Liu T, Liu Y, Chen S. Aerostatic lubrication. Harbin Institute of Technology press; 1990. p. 51–66.
- [24] A.H. Slocum, Precision Machine Design, Prentice-Hall, 1<sup>st</sup> edn., 1992.
- [25] M. Kanai, S. Ishihara, Bull. JSPE 56 1990. 2201–2207.
- [26] H.J. Sneck, J. Lub. Tech. 90 1968. 804–809.
- [27] B.C. Majumdar, *Wear* 36 1976. 269–273.
- [28] Wardle, F. (2015). *Ultra-Precision Bearings*. In Woodhead Publishing (1. Edition). Woodhead Publishing.
- [29] Bleuler, H., R. Clavel, J. M. Breguet, H. Langen and E. Pernette (2000). Issues in precision motion control and microhandling. *Proceedings-IEEE International Conference on Robotics and Automation*, 1(April), 959–964.
- [30] Gao, Q., L. Lu, W. Chen and G. Wang (2018). Optimal design of an annular thrust air bearing using parametric computational fluid dynamics model and genetic algorithms. *Proceedings of the Institution of Mechanical Engineers, Part J: Journal of Engineering Tribology* 232(10), 1203–1214.
- [31] Torralba, M., M. Valenzuela, J. A. Yagüe-Fabra, J. A. Albajez and J. J. Aguilar (2016). Large range nanopositioning stage design: A three-layer and two-stage platform. *Measurement: Journal of the International Measurement Confederation* 89, 55–71.

- [32] Khim, G. and C. H. Park, (2013). Analysis on the Static Performance of Vacuum-Preloaded Porous Air Bearings. *Journal of the Korean Society for Precision Engineering* 30(12), 1327–1333.
- [33] Ye, Y., X. Chen and X. Luo (2009). Dynamic characteristics of aerostatic bearings in nano-precision stage. *2009 International Conference on Information and Automation* 2003, 1050–1055.
- [34] Kwan, Y. B. P. and J. Corbett (1998). Porous aerostatic bearings-an updated review. *Wear*, 222(2), 69–73.
- [35] Schenk, C., S. Buschmann, S. Risse, R. Eberhardt and A. Tünnemann (2008). Comparison between flat aerostatic gas-bearing pads with orifice and porous feedings at high-vacuum conditions. *Precision Engineering* 32(4), 319–328.
- [36] Reynolds DB, Gross WA. Experimental investigation of whirl in self-acting air-lubricated journal bearings. *ASLE Trans* 1962;5:392–403. <https://doi.org/10.1080/05698196208972483>.
- [37] Malanoski SB. Experiments on an ultrastable gas journal bearing. *J Lubr Technol* 1967;89:433–8. <https://doi.org/10.1115/1.3617021>.
- [38] Waumans T, Peirs J, Al-Bender F, Reynaerts D. Aerodynamic journal bearing with a flexible, damped support operating at 7.2 million DN. *J Micro Micro* 2011;21: 104014. <https://doi.org/10.1088/0960-1317/21/10/104014>.
- [39] Waumans T, Peirs J, Reynaerts D, Al-Bender F. On the dynamic stability of high-speed gas bearings: Stability study and experimental validation. *Int J Sustain Constr Des* 2011;2:342–51. <https://doi.org/10.21825/scad.v2i2.20531>.
- [40] Matta P, Arghir M, Bonneau O. Experimental analysis of cylindrical air-bearing dynamic coefficients. *Tribol Trans* 2010;53:329–39. <https://doi.org/10.1080/10402000903283318>.
- [41] Cunningham RE, Fleming DP, Anderson WJ. Experimental stability studies of the herringbone-grooved gas-lubricated journal bearing. *J Lubr Technol* 1969;91: 52–7. <https://doi.org/10.1115/1.3554896>.
- [42] Cunningham RE, Fleming DP, Anderson WJ. Experimental load capacity and power loss of herringbone grooved gas lubricated journal bearings. *J Lubr Technol* 1971;93:415–22. <https://doi.org/10.1115/1.3451610>.
- [43] Heshmat H, Shapiro W, Gray S. Development of foil journal bearings for high load capacity and high-speed whirl stability. *J Lubr Technol* 1982;104:149–56. <https://doi.org/10.1115/1.3253173>.
- [44] Ku CPR, Heshmat H. Compliant foil bearing structural stiffness analysis – Part II: Experimental investigation. *J Tribol* 1993;115:364–9. <https://doi.org/10.1115/1.2921644>.
- [45] Heshmat H. Advancements in the performance of aerodynamic foil journal bearings: High speed and load capability. *J Tribol* 1994;116:287–94. <https://doi.org/10.1115/1.2927211>.
- [46] Heshmat H, Ku CPR. Structural damping of self-acting compliant foil journal bearings. *J Tribol* 1994;116:76–82. <https://doi.org/10.1115/1.2927050>.
- [47] Ku CPR, Heshmat H. Effects of static load on dynamic structural properties in a flexible supported foil journal bearing. *J Vib Acoust* 1994;116:257–62. <https://doi.org/10.1115/1.2930422>.
- [48] Dellacorte C, Lukaszewicz V, Valco MJ, Radil KC, Heshmat H. Performance and durability of high-temperature foil air bearings for oil-free turbomachinery. *Tribol Trans* 2000;43:774–80. <https://doi.org/10.1080/10402000008982407>.
- [49] Howard SA, Dellacorte C, Valco MJ, Prahl JM, Heshmat H. Steady-state stiffness of foil air journal bearings at elevated temperatures. *Tribol Trans* 2001;44: 489–93. <https://doi.org/10.1080/10402000108982486>.
- [50] Radil K, Howard S, Dykas B. The role of radial clearance on the performance of foil air bearings. *Tribol Trans* 2002;45:485–90. <https://doi.org/10.1080/10402000208982578>.
- [51] Radil KC, Dellacorte C. The effect of journal roughness and foil coatings on the performance of heavily loaded foil air bearings. *Tribol Trans* 2002;45:199–204. <https://doi.org/10.1080/10402000208982540>.
- [52] Salehi M, Heshmat H. Frictional dampers dynamic characterization-theory and experiments. *Tribology Ser* 2002;40:515–26. [https://doi.org/10.1016/S0167-8922\(02\)80057-8](https://doi.org/10.1016/S0167-8922(02)80057-8).
- [53] Salehi M, Heshmat H, Walton JF. On the frictional damping characterization of compliant bump foils. *J Tribol* 2003;125:804–13. <https://doi.org/10.1115/1.1575774>.
- [54] Salehi M, Heshmat H, Walton II JF. Advancements in the structural stiffness and damping of a large compliant foil journal bearing: An experimental study. *J Eng Gas Turbines Power* 2004;129:154–61. <https://doi.org/10.1115/1.2360598>.
- [55] Heshmat H, Walton II JF, Tomaszewski MJ. Demonstration of a turbojet engine using an air foil bearing. *Proc ASME Turbo Expo 2005: Power Land, Sea, Air* 2005;1:919–26. <https://doi.org/10.1115/gt2005-68404>.
- [56] DellaCorte C, Radil KC, Bruckner RJ, Howard SA. Design, fabrication, and performance of open source generation I and II compliant hydrodynamic gas foil

- bearings. *Tribol Trans* 2008;51:254–64. <https://doi.org/10.1080/10402000701772579>.
- [57] Kim TH, Andr es LS. Heavily loaded gas foil bearings: A model anchored to test data. *J Eng Gas Turbines Power* 2008;130:012504. <https://doi.org/10.1115/1.2770494>.
- [58] Kim TH, Lee J, Kim CH, Lee YB. Rotordynamic performance of an oil-free turbocharger supported on gas foil bearings: Effects of an assembly radial clearance. *Proc ASME Turbo Expo 2010: Power Land, Sea, Air 2010*;6:363–71. <https://doi.org/10.1115/gt2010-23243>.
- [59] Kim TH, Song JW, Lee YB, Sim K. Thermal performance measurement of a bump type gas foil bearing floating on a hollow shaft for increasing rotating speed and static load. *J Eng Gas Turbines Power* 2011;134:024501. <https://doi.org/10.1115/1.4004401>.
- [60] Ryu K, Andr es LS. Effect of cooling flow on the operation of a hot rotor-gas foil bearing system. *J Eng Gas Turbines Power* 2012;134:102511. <https://doi.org/10.1115/1.4007067>.
- [61] Sim K, Yong BL, Ho KT, Lee J. Rotordynamic performance of shimmed gas foil bearings for oil-free turbochargers. *J Tribol* 2012;134:031102. <https://doi.org/10.1115/1.4005892>.
- [62] Tian Y, Sun Y, Yu L. Structural stiffness and damping coefficients of a multi-leaf foil bearing with bump foils underneath. *J Eng Gas Turbines Power* 2013;136: 044501. <https://doi.org/10.1115/1.4026054>.
- [63] Sim K, Lee YB, Song JW, Kim JB, Kim TH. Identification of the dynamic performance of a gas foil journal bearing operating at high temperatures. *J Mech Sci Technol* 2014;28:43–51. <https://doi.org/10.1007/s12206-013-0945-6>.
- [64] Feng K, Liu Y, Zhao X, Liu W. Experimental evaluation of the structure characterization of a novel hybrid bump-metal mesh foil bearing. *J Tribol* 2015; 138:021702. <https://doi.org/10.1115/1.4031496>.
- [65] Andr es LS, Norsworthy J. Structural and rotordynamic force coefficients of a shimmed bump foil bearing: An assessment of a simple engineering practice. *J Eng Gas Turbines Power* 2015;138:012505. <https://doi.org/10.1115/1.4031238>.
- [66] Hoffmann R, Liebich R. Experimental and numerical analysis of the dynamic behaviour of a foil bearing structure affected by metal shims. *Tribol Int* 2017;115: 378–88. <https://doi.org/10.1016/j.triboint.2017.04.040>.
- [67] Zywica G, Bagi nski P, Kici nski J. Selected operational problems of high-speed rotors supported by gas foil bearings. *Tech Mech Sci J Fundam Appl Eng Mech* 2017;37:339–46. <https://doi.org/10.24352/UB.OVGU-2017-109>.
- [68] Feng K, Guan HQ, Zhao ZL, Liu TY. Active bump-type foil bearing with controllable mechanical preloads. *Tribol Int* 2018;120:187–202. <https://doi.org/10.1016/j.triboint.2017.12.029>.
- [69] Guo Z, Peng L, Feng K, Liu W. Measurement and prediction of nonlinear dynamics of a gas foil bearing supported rigid rotor system. *Measurement* 2018;121: 205–17. <https://doi.org/10.1016/j.measurement.2017.12.039>.
- [70] Hoffmann R, Liebich R. Characterisation and calculation of nonlinear vibrations in gas foil bearing systems—an experimental and numerical investigation. *J Sound Vib* 2018;412:389–409. <https://doi.org/10.1016/j.jsv.2017.09.040>.
- [71] Zhang B, Qi S, Feng S, Geng H, Sun Y, Yu L. An experimental investigation of a microturbine simulated rotor supported on multileaf gas foil bearings with backing bump foils. *Proc IME J J Eng Tribol* 2018;232:1169–80. <https://doi.org/10.1177/1350650117725463>.
- [72] Sim K, Kim TH. Thermohydrodynamic analysis of bump-type gas foil bearings using bump thermal contact and inlet flow mixing models. *Tribol Int* 2012;48: 137–48. <https://doi.org/10.1016/j.triboint.2011.11.017>.
- [73] Feng K, Kaneko S. A thermohydrodynamic sparse mesh model of bump-type foil bearings. *J Eng Gas Turbines Power* 2013;135:022501. <https://doi.org/10.1115/1.4007728>.
- [74] DellaCorte C, Zaldana AR, Radil KC. A systems approach to the solid lubrication of foil air bearings for oil-free turbomachinery. *J Tribol* 2004;126:200–7. <https://doi.org/10.1115/1.1609485>.
- [75] Rubio D, Andr es LS. Structural stiffness, dry friction coefficient, and equivalent viscous damping in a bump-type foil gas bearing. *J Eng Gas Turbines Power* 2006; 129:494–502. <https://doi.org/10.1115/1.2360602>.
- [76] Rubio D, Andr es LS. Bump-type foil bearing structural stiffness: Experiments and predictions. *J Eng Gas Turbines Power* 2006;128:653–60. <https://doi.org/10.1115/1.2056047>.
- [77] Andr es LS, Kim TH. Forced nonlinear response of gas foil bearing supported rotors. *Tribol Int* 2008;41:704–15. <https://doi.org/10.1016/j.triboint.2007.12.009>.
- [78] Shrestha SK, Kim D, Kim YC. Experimental feasibility study of radial injection cooling of three-pad air foil bearings. *J Tribol* 2013;135:041703. <https://doi.org/10.1115/1.4024547>.

- [79] Lee YB, Park DJ, Kim CH, Kim SJ. Operating characteristics of the bump foil journal bearings with top foil bending phenomenon and correlation among bump foils. *Tribol Int* 2008;41:221–33. <https://doi.org/10.1016/j.triboint.2007.07.003>.
- [80] Andr es LS, Kim TH. Thermohydrodynamic analysis of bump type gas foil bearings: A model anchored to test data. *J Eng Gas Turbines Power* 2010;132:042504. <https://doi.org/10.1115/1.3159386>.
- [81] Andr es LS, Ryu K, Kim TH. Thermal management and rotordynamic performance of a hot rotor-gas foil bearings system – part II: Predictions versus test data. *J Eng Gas Turbines Power* 2011;133:062502. <https://doi.org/10.1115/1.4001827>.
- [82] Ryu K, Ashton Z. Bump-type foil bearings and flexure pivot tilting pad bearings for oil-free automotive turbochargers: Highlights in rotordynamic performance. *J Eng Gas Turbines Power* 2015;138:042501. <https://doi.org/10.1115/1.4031440>.
- [83] Bonneau D, Absi J. Analysis of aerodynamic journal bearings with small number of herringbone grooves by finite element method. *J Tribol* 1994;116:698–704. <https://doi.org/10.1115/1.2927320>.
- [84] Faria MTC. Some performance characteristics of high speed gas lubricated herringbone groove journal bearings. *JSME Int J C-Mech Sy* 2001;44:775–81. <https://doi.org/10.1299/jsmec.44.775>.
- [85] Kim D, Lee S, Bryant MD, Ling FF. Hydrodynamic performance of gas microbearings. *J Tribol* 2004;126:711–8. <https://doi.org/10.1115/1.1792676>.
- [86] Pan C.H.T., Kim D. Stability characteristics of a rigid rotor supported by a gas lubricated spiral-groove conical bearing. *Proceedings of the STLE/ASME 2006 International Joint Tribology Conference, 2006*; 1271–1279. <https://doi.org/10.1115/IJTC2006-12105>.
- [87] Chu LM, Li WL, Shen RW, Tsai TI. Dynamic characteristics of grooved air bearings in microsystems. *Proc IME J J Eng Tribol* 2009;223:895–908. <https://doi.org/10.1243/13506501jet517>.
- [88] Rashidi R, Mohammadi KA, Bakhtiari-Nejad F. Effect of bearing number on non-linear dynamic behaviour of aerodynamic non-circular journal bearing systems. *Proc IME J J Eng Tribol* 2010;224:139–56. <https://doi.org/10.1243/13506501jet645>.
- [89] Schiffmann J, Favrat D. Integrated design and optimization of gas bearing supported rotors. *J Mech Des* 2010;132:051007. <https://doi.org/10.1115/1.4001381>.
- [90] Miyanaga N, Tomioka J. Stability analysis of herringbone-grooved aerodynamic journal bearings for ultra high-speed rotations. *Int J Mater Mech Manuf* 2016;4: 156–61. <https://doi.org/10.7763/IJMMM.2016.V4.246>.
- [91] Du J, Zhu J, Li B, Liu D, Song C. The effect of area contact on the static performance of multileaf foil bearings. *Tribol Trans* 2015;58:592–601. <https://doi.org/10.1080/10402004.2014.997907>.
- [92] Li Y, Lei G, Sun Y, Wang L. Effect of environmental pressure enhanced by a booster on the load capacity of the aerodynamic gas bearing of a turbo expander. *Tribol Int* 2017;105:77–84. <https://doi.org/10.1016/j.triboint.2016.09.027>.
- [93] Laouadi B, Lahmar M, Saïd BB, Mouassa A, Boucherit H. Analysis of couple-stress effects in gas foil bearings using the vk stokes micro-continuum theory. *Lubr Sci* 2018;30:401–39. <https://doi.org/10.1002/ls.1430>.
- [94] Bonello P. The effects of air film pressure constraints and top foil detachment on the static equilibrium, stability and modal characteristics of a foil-air bearing rotor model. *J Sound Vib* 2020;485:115590. <https://doi.org/10.1016/j.jsv.2020.115590>.
- [95] Gu Y, Ren G, Zhou M. A fully coupled elasto-hydrodynamic model for static performance analysis of gas foil bearings. *Tribol Int* 2020;147:106297. <https://doi.org/10.1016/j.triboint.2020.106297>.
- [96] Baum C, Hetzler H, Schr oders S, Leister T, Seemann W. A computationally efficient nonlinear foil air bearing model for fully coupled, transient rotor dynamic investigations. *Tribol Int* 2021;153:106434. <https://doi.org/10.1016/j.triboint.2020.106434>.
- [97] Yongpeng G, Xudong L, Gexue R, Ming Z. An efficient three-dimensional foil structure model for bump-type gas foil bearings considering friction. *Friction* 2021;9:1450–63. <https://doi.org/10.1007/s40544-020-0427-7>.
- [98] Zhao X, Xiao S. A three-dimensional model of gas foil bearings and the effect of misalignment on the static performance of the first and second generation foil bearings. *Tribol Int* 2021;156:106821. <https://doi.org/10.1016/j.triboint.2020.106821>.
- [99] Radil KC, Dellacorte C. A three-dimensional foil bearing performance map applied to oil-free turbomachinery. *Tribol Trans* 2010;53:771–8. <https://doi.org/10.1080/10402001003797942>.
- [100] Li C, Du J, Zhu J, Yao Y. Effects of structural parameters on the load carrying capacity of the multi-leaf gas foil journal bearing based on contact mechanics. *Tribol Int* 2019;131:318–31. <https://doi.org/10.1016/j.triboint.2018.09.003>.
- [101] Ha DN, Stolarski TA, Yoshimoto S. An aerodynamic bearing with adjustable geometry and self-lifting

- capacity. Part 1: Self-lift capacity by squeeze film. Proc IME J J Eng Tribol 2005;219:33-9. <https://doi.org/10.1243/135065005x9682>.
- [102] Song J, Kim D. Foil gas bearing with compression springs: Analyses and experiments. J Tribol 2007;129:628-39. <https://doi.org/10.1115/1.2736455>.
- [103] Andr es LS, Chirathadam TA, Ryu K, Kim TH. Measurements of drag torque, lift-off journal speed, and temperature in a metal mesh foil bearing. J Eng Gas Turbines Power 2010;132:112503. <https://doi.org/10.1115/1.4000863>.
- [104] Feng K, Zhao X, Huo C, Zhang Z. Analysis of novel hybrid bump-metal mesh foil bearings. Tribol Int 2016;103:529-39. <https://doi.org/10.1016/j.triboint.2016.08.008>.
- [105] Mahner M, Bauer M, Lehn A, Schweizer B. An experimental investigation on the influence of an assembly preload on the hysteresis, the drag torque, the lift-off speed and the thermal behavior of three-pad air foil journal bearings. Tribol Int 2019;137:113-26. <https://doi.org/10.1016/j.triboint.2019.02.026>.
- [106] Li C, Du J, Yao Y. Study of load carrying mechanism of a novel three-pad gas foil bearing with multiple sliding beams. Mech Syst Signal Process 2020;135:106372. <https://doi.org/10.1016/j.ymssp.2019.106372>.
- [107] Lee YB, Kim CH, Kim TH, Kim TY. Effects of mesh density on static load performance of metal mesh gas foil bearings. J Eng Gas Turbines Power 2011; 134:012502. <https://doi.org/10.1115/1.4004142>.
- [108] Guan HQ, Feng K, Cao YL, Huang M, Wu YH, Guo ZY. Experimental and theoretical investigation of rotordynamic characteristics of a rigid rotor supported by an active bump-type foil bearing. J Sound Vib 2019;115049. <https://doi.org/10.1016/j.jsv.2019.115049>.
- [109] Hu H, Feng M, Ren T. Study on the performance of gas foil journal bearings with bump-type shim foil. Proc IME J J Eng Tribol 2020;0. <https://doi.org/10.1177/1350650120969003>.
- [110] Bouchehit B, Saïd BB, Garcia M. Static and dynamic performances of refrigerant-lubricated bearings. Tribol Int 2016;96:326-48. <https://doi.org/10.1016/j.triboint.2015.12.035>.
- [111] Antonín Skarolek, Numerical Analysis of Rotor Systems with Aerostatic Journal Bearings, Dissertation submitted to Technical University of Liberec on January 2012.
- [112] Qi Zhao , Mingchen Qiang , Yu Hou, Shuangtao Chen, Tianwei Lai. Research Developments of Aerostatic Thrust Bearings: A Review, Appl. Sci. 2022, 12, 11887. <https://doi.org/10.3390/app122311887>